

Verification of NIMROD's Rosenbluth potentials*

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NIMROD team zoom meeting, Nov 1, 2021

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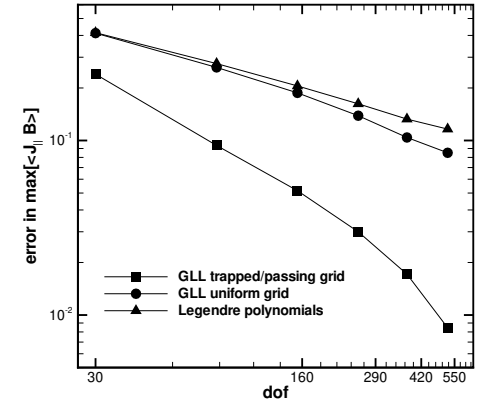
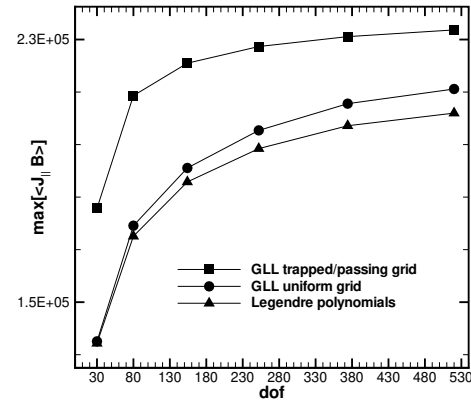
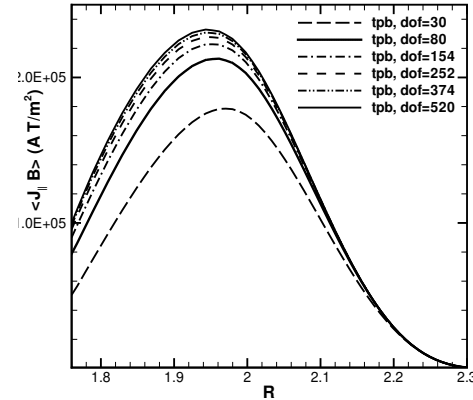
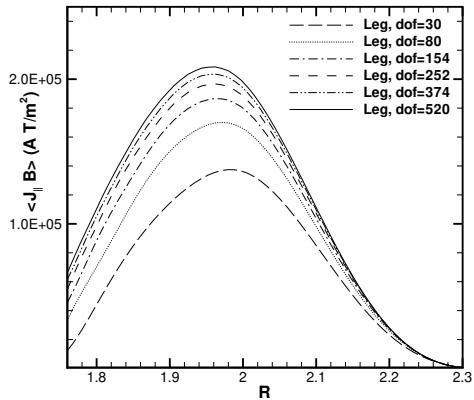
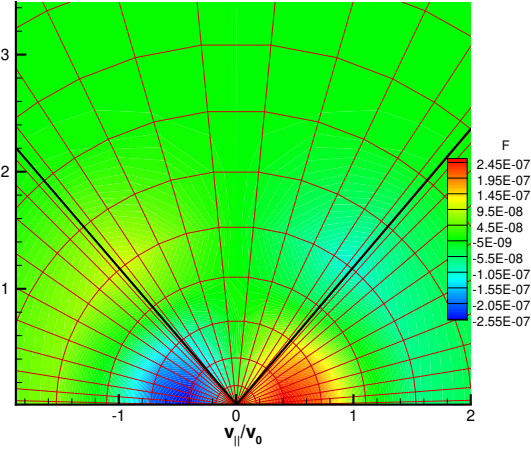
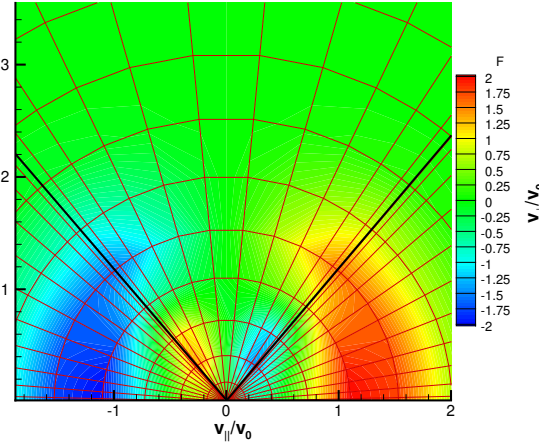
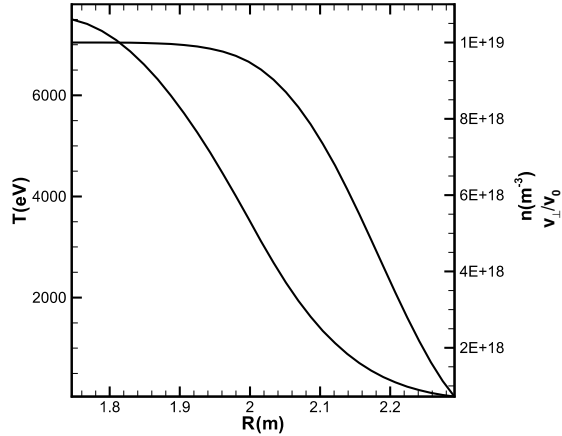
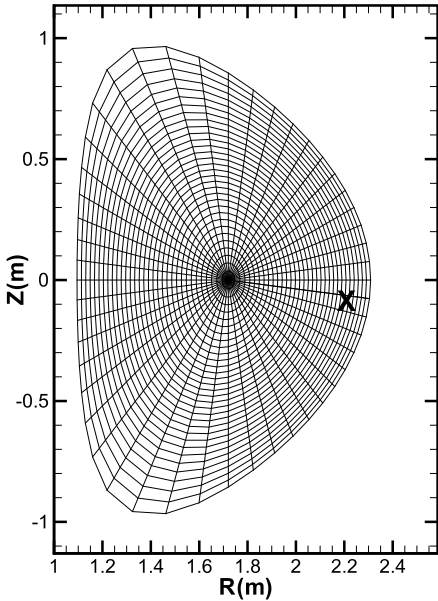
Verification of NIMROD's Rosenbluth potentials

Tests added to manuscript submitted to JCP in February:

- 1) Convergence of Bootstrap current
- 2) Poisson's equation using method of manufactured solutions
- 3) Sauter coefficient comparison (*tpb* GLL vs Legendre)
Landreman and Ernst, JCP 243 (2013)

FE pitch-angle basis improves bootstrap current

$$\mathbf{v}_{\parallel} \cdot \left[\nabla F - \frac{1 - \xi^2}{2\xi} \nabla \ln B \frac{\partial F}{\partial \xi} \right] - C(F) = -\mathbf{v}_D \cdot \left(\nabla \ln n_0 - \left(\frac{3}{2} - s^2 \right) \nabla \ln T_0 \right) f_0 \quad \langle J_{\parallel} B \rangle = \sum_b q_b \left\langle B \int dv_{\parallel} F_b \right\rangle$$



Solving Poisson's equation using method of manufactured solutions

The axisymmetric Coulomb collision field operator:

$$C \left[f_a^M, F_b \right] = \Gamma_{ab} f_a^M \left\{ 4\pi \frac{m_a}{m_b} F_b - \frac{2H_b}{v_{Ta}^2} + \left(\frac{m_a}{m_b} - 1 \right) \frac{2v}{v_{Ta}^2} \frac{\partial H_b}{\partial v} + \frac{2v^2}{v_{Ta}^4} \frac{\partial^2 G_b}{\partial v^2} \right\}$$

Normalize speed $s \equiv v/v_{Ta}$, speed collocation method and pitch-angle FEM:

$$\nabla_v^2 H_b = -4\pi F_b$$

$$F_a(v_{Ta}s, \xi') = \sum_{l'} F_{a,l'}(v_{Ta}s) Q_{l'}(\xi')$$

$$F_{a,l'}(v_{Ta}s) = \sum_{k=1}^{N_s} F_{a,l',k} L_k(s) e^{-s^2}$$

$$\int_0^\infty ds L_j(s) L_k(s) e^{-s^2} = \delta_{jk}$$

$$F_{a,l'}(v_{Ta}s) = \sum_{k=1}^{N_s} \sum_j w_j L_{k'}(s_j) F_{a,l'}(v_{Ta}s_j) L_k(s) e^{-s^2}$$



$$\int_{-1}^1 d\xi H_b(v_{Ta}s_i, \xi) Q_l(\xi) = v_{Ta}^2 s_i^2 \sum_{l'} \sum_j H_{a,b,l,i,l',j} F_{b,l'}(v_{Tb}s_j)$$

$$\int_{-1}^1 d\xi \frac{\partial H_b}{\partial v}(v_{Ta}s_i, \xi) Q_l(\xi) = v_{Ta} s_i \sum_{l'} \sum_j H'_{a,b,l,i,l',j} F_{b,l'}(v_{Tb}s_j)$$

$$\int_{-1}^1 d\xi \frac{\partial^2 G_b}{\partial v^2}(v_{Ta}s_i, \xi) Q_l(\xi) = v_{Ta}^2 s_i^2 \sum_{l'} \sum_j G''_{a,b,l,i,l',j} F_{b,l'}(v_{Tb}s_j)$$

where $H_{a,b,l,i,l',j}$, $H'_{a,b,l,i,l',j}$, and $G''_{a,b,l,i,l',j}$ are precomputed coupling arrays

Solving Poisson's equation using method of manufactured solutions

1) Starting with exact solution we want to reproduce:

$$H(v, \xi) = \exp \left\{ - \left[\theta_{\parallel}^{-1} \xi^2 + \theta_{\perp}^{-1} (1 - \xi^2) \right] \left(\frac{v}{v_{\top}} \right)^2 \right\}$$

2) Let operator $\nabla_v^2 H = -4\pi F$ act on solution to produce RHS:

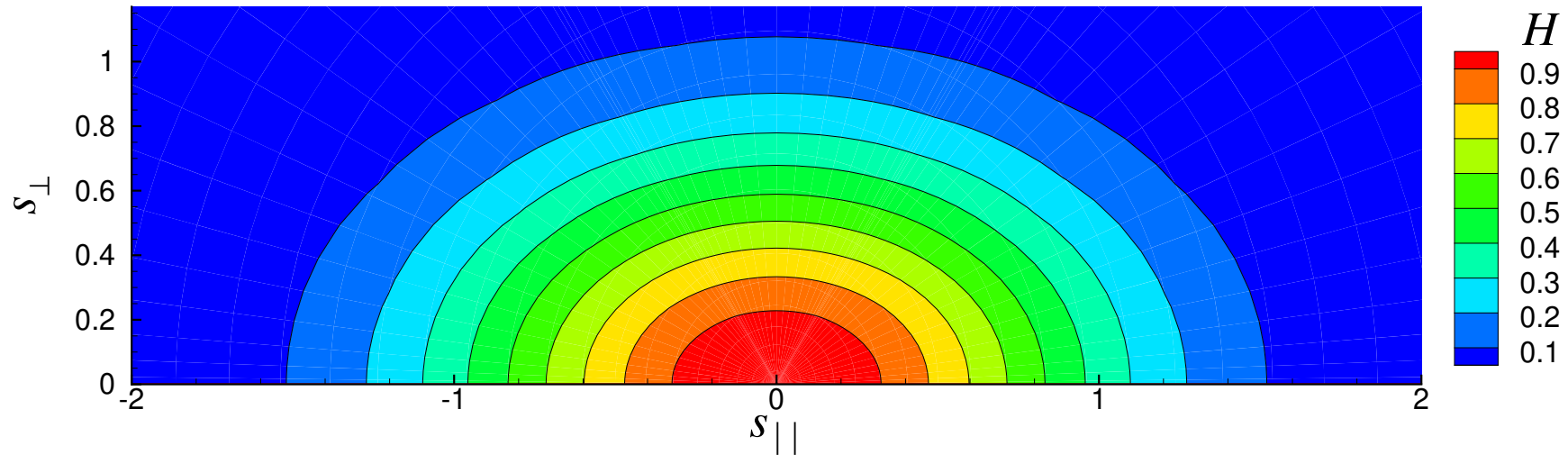
$$F(v, \xi) = \frac{1}{2\pi v_{\top}^2} \left[\theta_{\parallel}^{-1} + 2\theta_{\perp}^{-1} - 2\theta_{\parallel}^{-2} \xi^2 \left(\frac{v}{v_{\top}} \right)^2 - 2\theta_{\perp}^{-2} (1 - \xi^2) \left(\frac{v}{v_{\top}} \right)^2 \right] H(v, \xi)$$

3) Project RHS onto basis and solve equation to obtain numerical approximate to solution.

$$H(v_{\top} s_i, \xi_k) = \sum_l [M^{-1}]_{kl} \boxed{\int_{-1}^1 d\xi H(v_{\top} s_i, \xi) Q_l(\xi)} \quad \text{where} \quad M_{kl} \equiv \int_{-1}^1 d\xi Q_k(\xi) Q_l(\xi)$$

Solving Poisson's equation using method of manufactured solutions

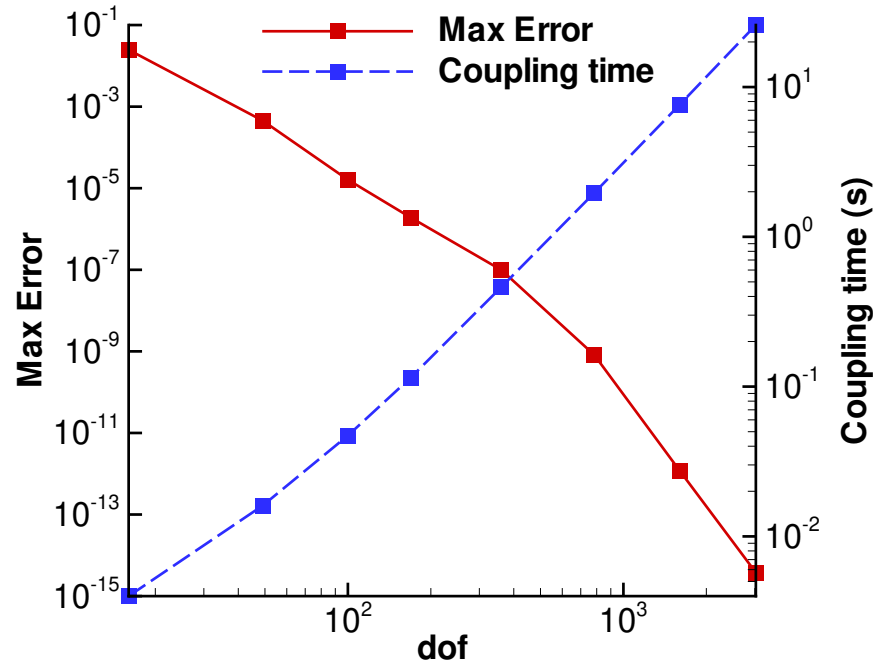
$$H = \exp \left[- \left(s_{\parallel}^2 + 2s_{\perp}^2 \right) \right]$$



$$(N_s, p) = (55, 18)$$

Solving Poisson's equation using method of manufactured solutions

$$\text{Max Error} = \max_{i,l} \left| s_i^2 \sum_{l'} \sum_j H_{l,i,l',j} v_{\top}^2 F_{l'}(v_{\top} s_j) - \int_{-1}^1 d\xi \exp \left\{ - \left[\xi^2 s_i^2 + 2 (1 - \xi^2) s_i^2 \right] \right\} Q_l(\xi) \right|$$

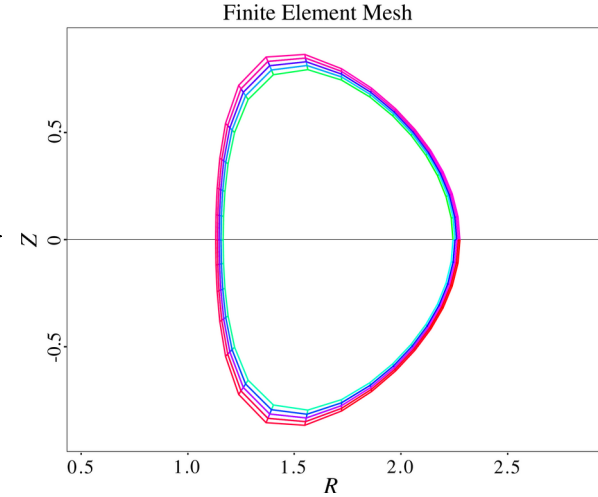
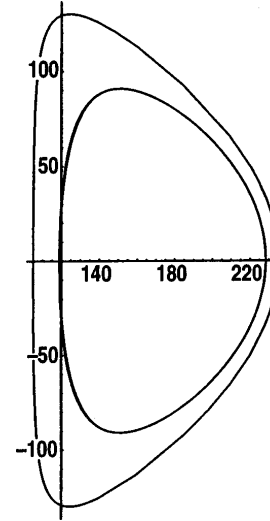


$$(N_s, p) = (4, 1), (7, 2), (10, 3), (13, 4), (19, 6), (28, 9), (40, 13), (55, 18)$$

L_{32} Sauter coefficient (*tpb* GLL vs Legendre)

$$\langle \mathbf{j} \cdot \mathbf{B} \rangle = -cRB_\phi p_e \left[\mathcal{L}_{31} \frac{1}{p_e} \left(\frac{dp_e}{d\psi} + \frac{dp_i}{d\psi} \right) + \frac{\mathcal{L}_{32}}{T_e} \frac{dT_e}{d\psi} + \frac{\mathcal{L}_{34}\alpha}{ZT_e} \frac{dT_i}{d\psi} \right]$$

$$\mathcal{L}_{32} = -4\pi^{-1/2} \left\langle \hat{B} \int_{-1}^1 d\xi \int_0^\infty ds s^3 \xi f_{e1}^{(T_e)} \right\rangle$$

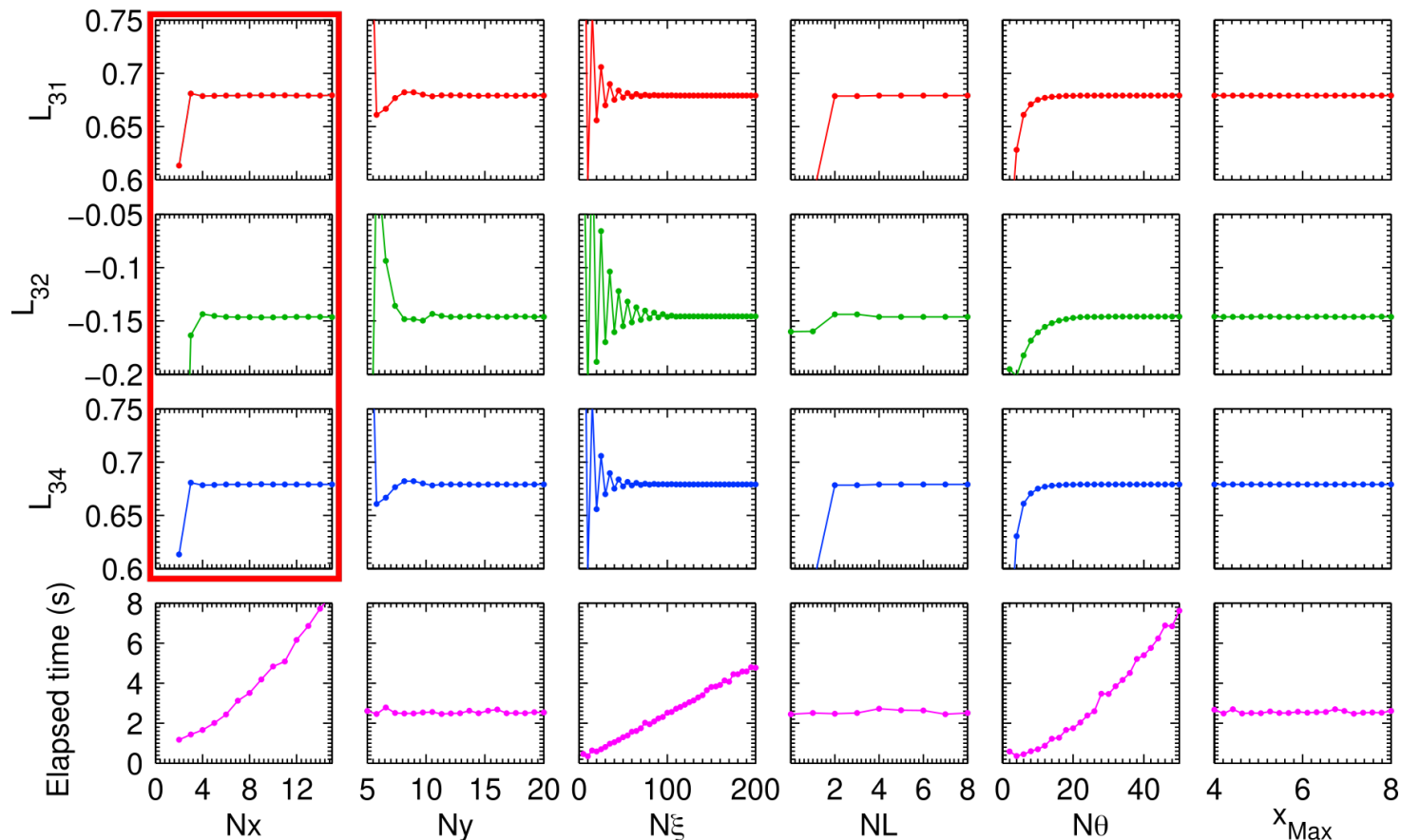


$$s\xi \frac{\partial f_{e1}^{(T_e)}}{\partial \theta} - \frac{(1 - \xi^2)s}{2\hat{B}} \left(\frac{\partial \hat{B}}{\partial \theta} \right) \frac{\partial f_{e1}^{(T_e)}}{\partial \xi} - \frac{v'}{qR_0 \mathbf{b} \cdot \nabla \theta} \hat{C} = \frac{1 + \xi^2}{2} s^2 \left(s^2 - \frac{5}{2} \right) e^{-s^2} \frac{1}{\hat{B}^2} \frac{\partial \hat{B}}{\partial \theta}$$

See M. Landreman, D. R. Ernst, J. Comput. Phys. 243 (2013).

R. L. Miller, M. S. Chu, J. M. Greene, Y. R. Lin-Liu, and R. E. Waltz, Phys. Plasmas 5, 973 (1998).

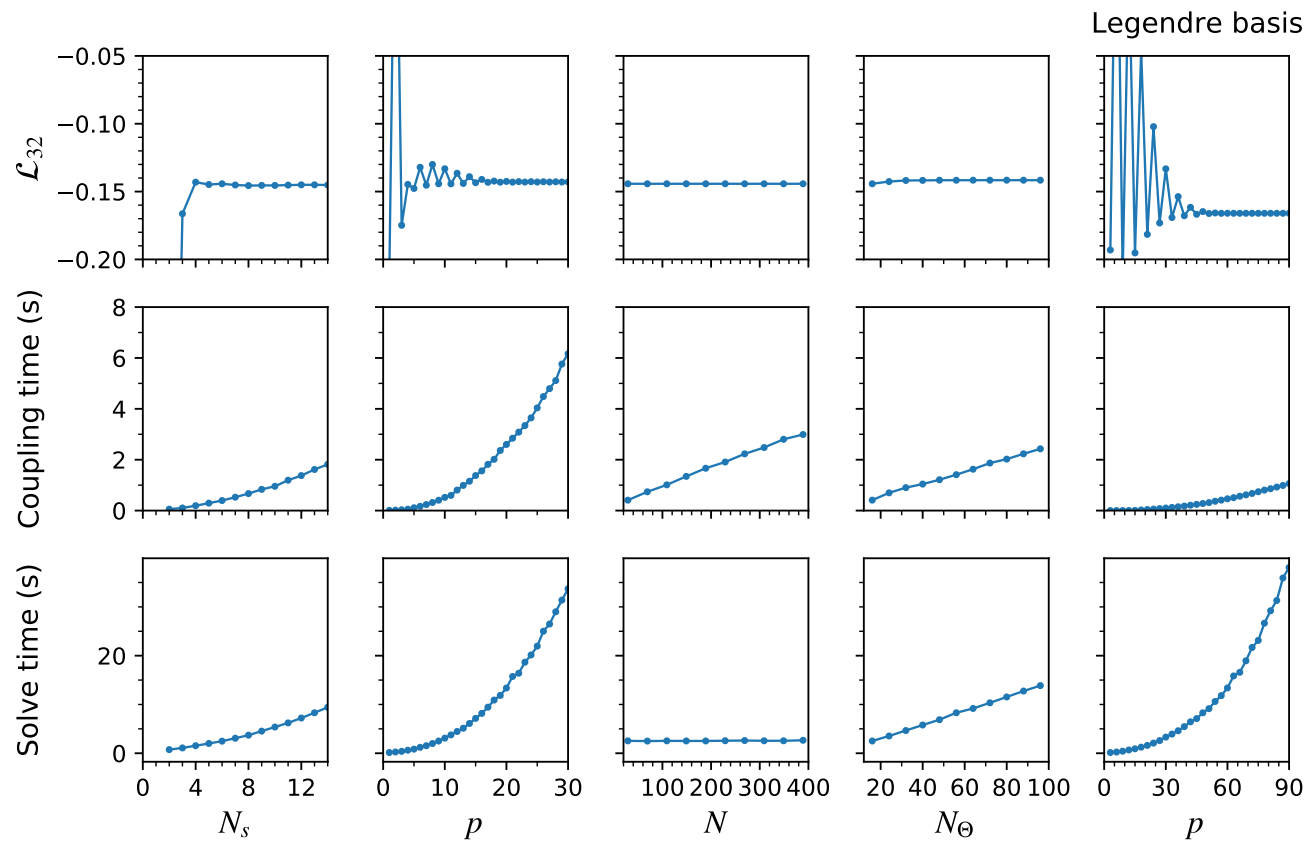
L_{32} Sauter coefficient (*tpb* GLL vs Legendre)



Except for quantities being scanned, $N_x = 6$, $N_y = 20$, $N_\xi = 100$, $N_L = 4$, $N_\theta = 25$, and $x_{Max} = 5$.

Figure taken from M. Landreman, D. R. Ernst, J. Comput. Phys. 243 (2013).

L_{32} Sauter coefficient (*tpb* GLL vs Legendre)



Except for quantities being scanned, $N_s = 6$, $p = 9$, $N = 29$, $N_\Theta = 16$.

Summary

We've improved NIMROD's axisymmetric Coulomb collision field operator

Tests:

- Low order collisional moments
- Bootstrap current using different pitch-angle bases adds to the story in 2015 PoP paper[†]

Two new verification tests added

- “Poison solve”, H, tested with method of manufactured solutions
- L_{32} Sauter coefficient calculation

Bootstrap current computed with higher resolution and convergence shown with error plot