

NIMROD simulations of Innovative Confinement Concepts

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Motivation

- inspired by successful SSPX simulations of coaxial flux injection and sustainment^a
- coplanar flux injection is used in several ICC experiments (e.g. P. Bellan's experiment^b, Woodruff Scientific)
- study physics and numerics of helicity injection and flux amplification
- simulations will help improve operation and efficiency by elucidating physical processes of injection, columnation, reconnection, and flux amplification

^aHooper, E. B., et al., "NIMROD resistive magnetohydrodynamic simulations of spheromak physics", PoP **15**, 2008

^bHsu and Bellan, "On Jets, Kinks, and spheromaks formed by a planar magnetized coaxial gun", PoP **12**, 2005



NIMROD^a (NonIdeal MHD with Rotation - Open Discussion)

- massively parallel 3-D MHD simulation
- finite elements in poloidal plane and Fourier modes in toroidal direction → axisymmetric geometry
- utilizes Lagrange type quadrilateral structured finite elements in 2-D
- can handle extreme anisotropies, $\frac{\chi_{\parallel}}{\chi_{\perp}} \gg 1$
- flexibility to model general geometry → real experiments
- model experiment relevant parameters, $S > 10^7$
- semi-implicit advance, not restricted by magnetosonic CFL condition
- assumes a steady state background and evolves perturbed quantities
→ $A(\mathbf{x}, t) = A_s(\mathbf{x}) + \delta A(\mathbf{x}, t)$
- allows linear and nonlinear simulations



NIMROD equations

- NIMROD evolves the **extended** MHD equations

$$\frac{\partial \mathbf{B}}{\partial t} = -\nabla \times \mathbf{E}$$

$$\nabla \times \mathbf{B} = \mu_0 \mathbf{J}$$

$$\mathbf{E} = -\mathbf{U} \times \mathbf{B} + \eta \mathbf{J} + \frac{1}{ne} \mathbf{J} \times \mathbf{B}$$

$$+ \frac{m_e}{ne^2} \left[\frac{\partial \mathbf{J}}{\partial t} + \nabla \cdot (\mathbf{J}\mathbf{U} + \mathbf{U}\mathbf{J}) \right]$$

$$+ \sum_{\alpha} \frac{q_{\alpha}}{m_{\alpha}} (\nabla p_{\alpha} + \nabla \cdot \Pi_{\alpha})$$

$$\frac{\partial n}{\partial t} + \nabla \cdot (n\mathbf{U}) = \nabla \cdot D\nabla n$$

$$mn \left(\frac{\partial \mathbf{U}}{\partial t} + \mathbf{U} \cdot \nabla \mathbf{U} \right) = \mathbf{J} \times \mathbf{B} - \nabla p - \nabla \cdot \Pi - \nabla \cdot p_h$$

$$\frac{n_{\alpha}}{\gamma - 1} \left(\frac{\partial T_{\alpha}}{\partial t} + \mathbf{U}_{\alpha} \cdot \nabla T_{\alpha} \right) = -\nabla \cdot q_{\alpha} + Q_{\alpha}$$

$$-p_{\alpha} \nabla \cdot \mathbf{U}_{\alpha} - \Pi_{\alpha} : \nabla \mathbf{U}_{\alpha}$$

Inductive Flux Injection Model

- NIMROD has two available flux injection models^a
 - direct flux injection via Faraday’s law (specifying tangential \mathbf{E} field at the boundary)
 - inductive flux injection via Ampere’s law (specifying a tangential \mathbf{B} field at the boundary)
- inductive flux injection (i.e. specifying input current) is closer to (coaxial gun source) experiment
- exploit integral Ampere’s law $\oint \mathbf{B} \cdot d\mathbf{l} = \mu_0 I$
- specify B_ϕ at the boundary corresponding to coaxial gap to induce poloidal current in simulation domain

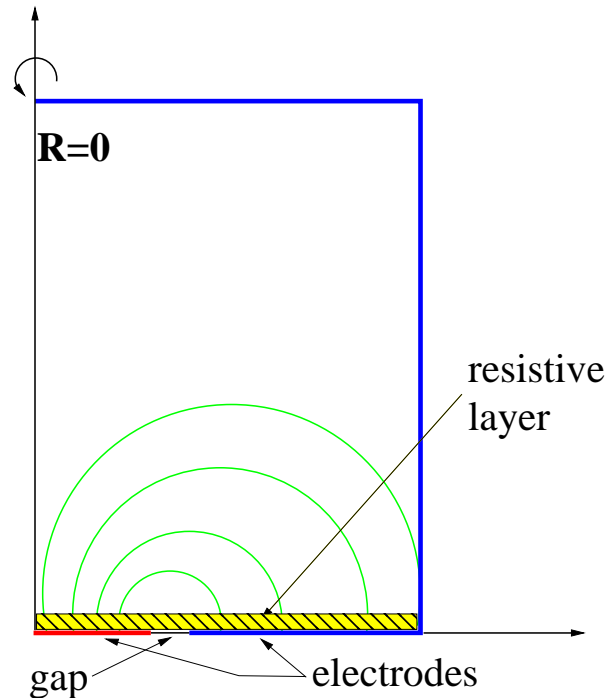
^aC. Sovinec, “Ohmic Current Drive in NIMROD Simulation”, NIMROD internal note, 2005

Inductive Flux Injection Model cont.

- along the boundary corresponding to flux gap specify $B_\phi R$
 - otherwise boundary condition is no-slip perfect conductor
- prescribed $B_\phi R$ induces a poloidal current in the simulation domain
- amplitude of $B_\phi R$ may vary with time (e.g. constant slope or programmed from experiment)
- ? thin highly resistive layer along bottom to rapidly diffuse flux across bottom
- the resulting $\mathbf{J} \times \mathbf{B}$ force pulls in the flux, drives columnation

Coplanar Flux Injection Simulation

- cylindrical vessel with small flux gap of a few centimeters

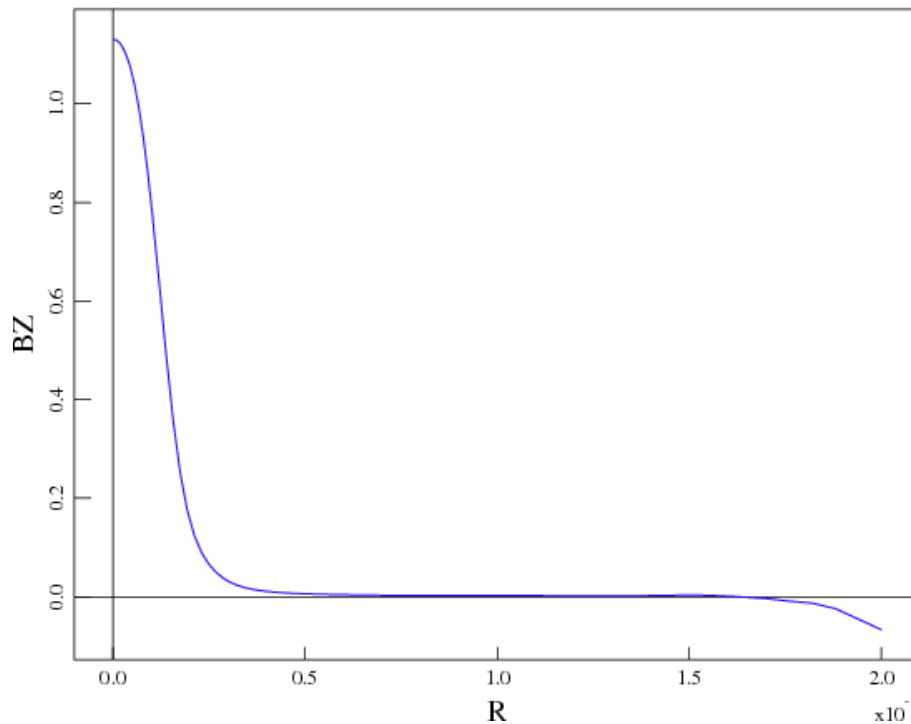


- vacuum field is dipole-like $\sim 1mWb$
 - flux gap located at top of the arc
- peak current is $40 - 100kA$ ramped over $1 - 10\mu s$
- thin highly resistive layer across bottom 10^5 larger than background resistivity

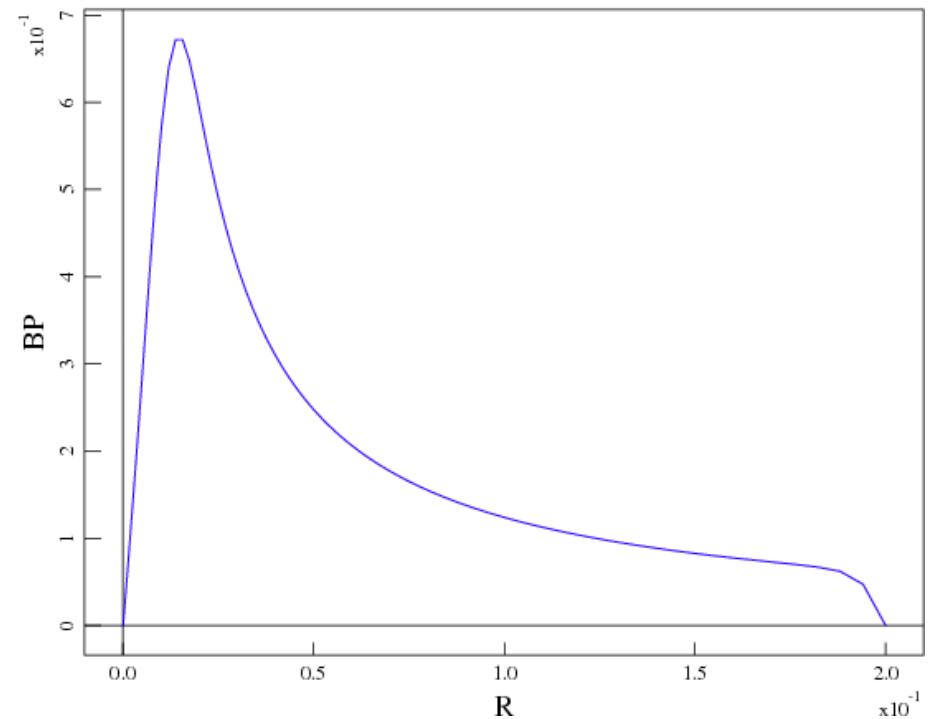
Formation of Axisymmetric Screw Pinch

- domain is cylinder radius 20cm , height 25cm , electrode gap at $[5.5\text{cm}, 6\text{cm}]$
- density 1×10^{19} , $v_A \simeq .5 \times 10^6$, 1mWb
- current ramped over $5\mu\text{s}$ to 80kA and flat topped, $\lambda_{gun} \simeq 90$

Re Bz vs. i



Re Bphi vs. i



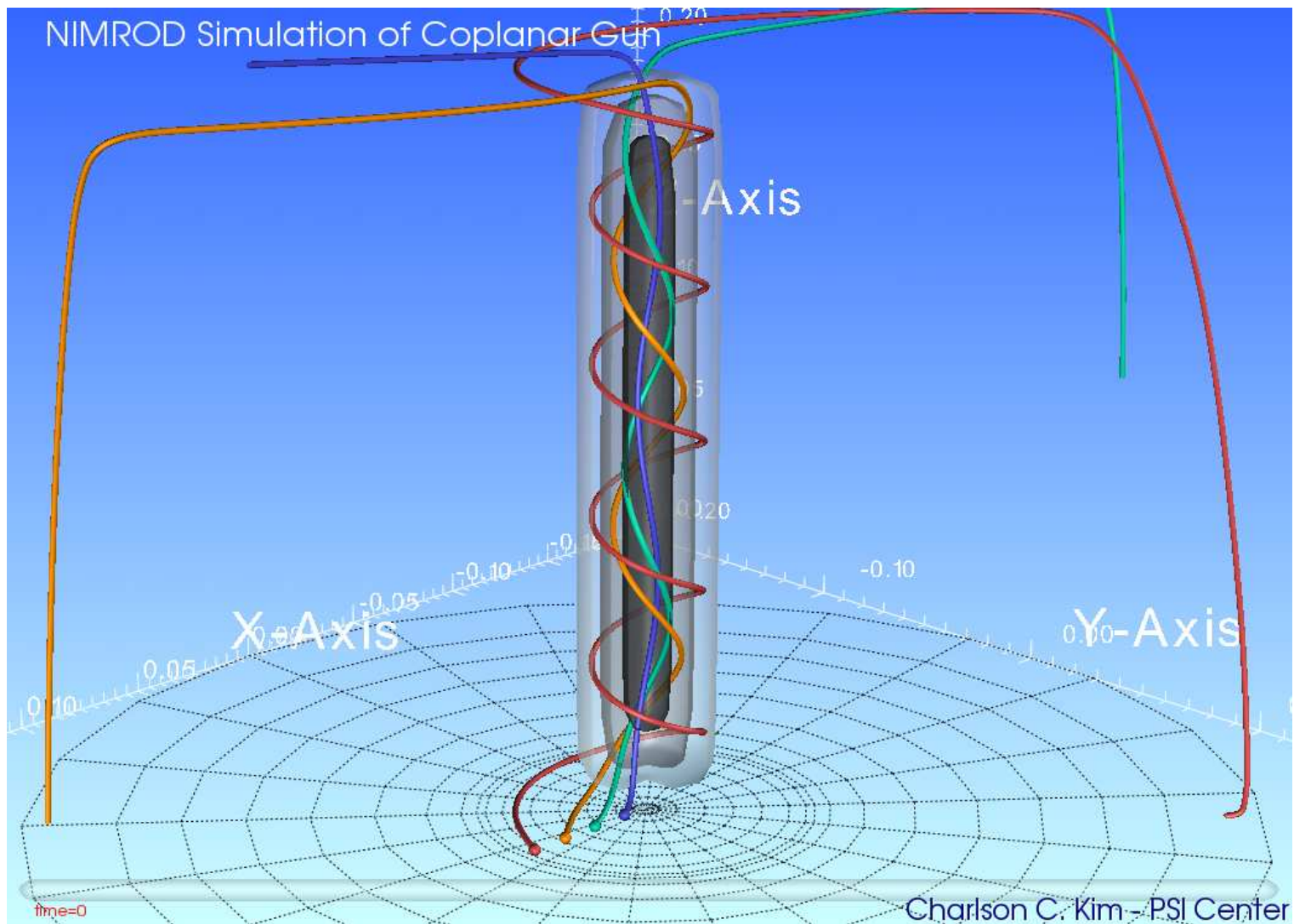


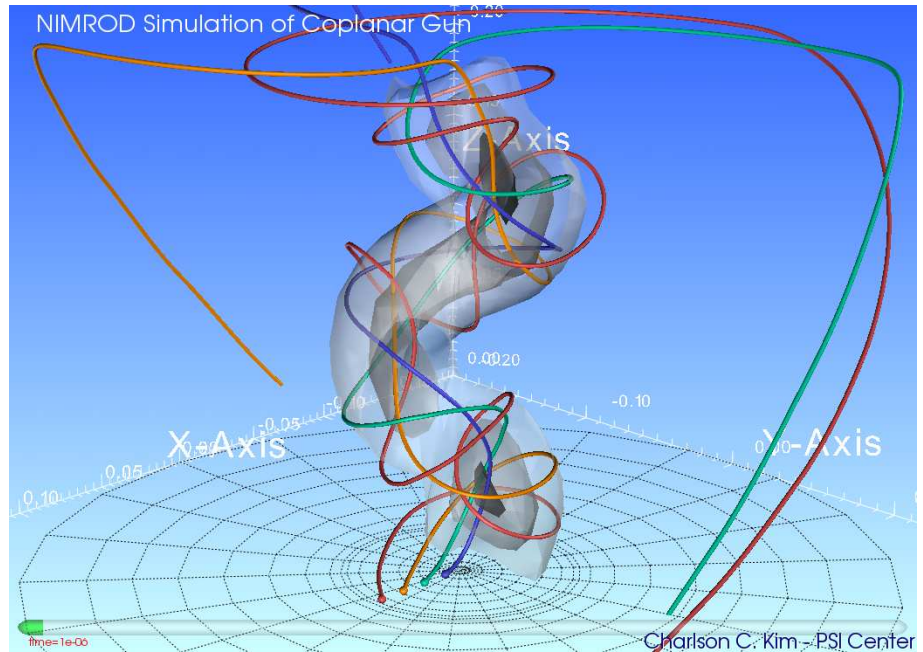
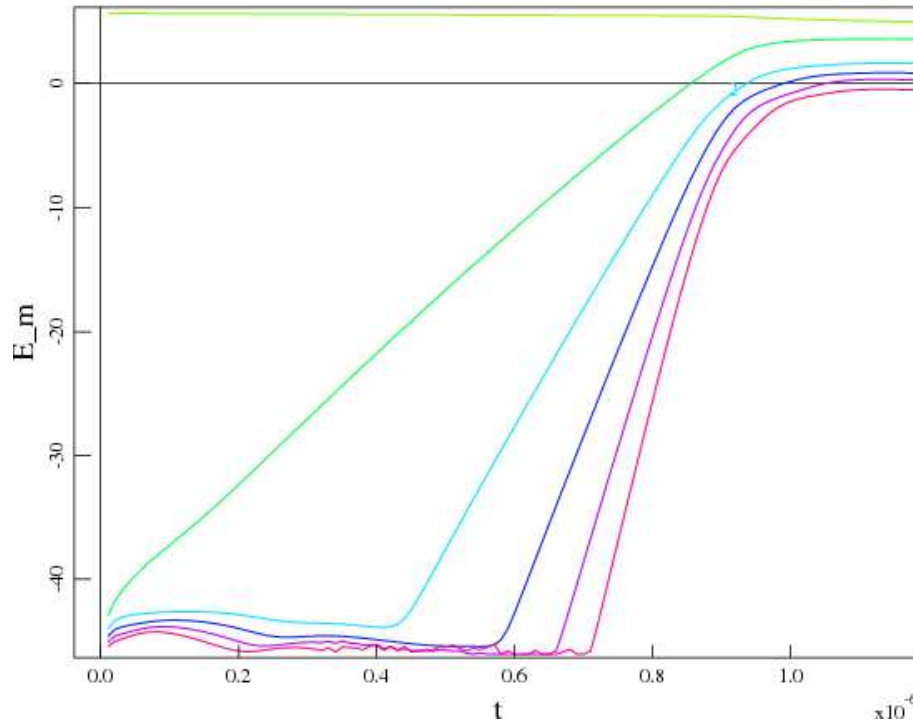
Figure 1: screw pinch - contours $[\.3, \.6, \.9]|B|_{max}$ with field lines

- serves as initial condition for subsequent simulations

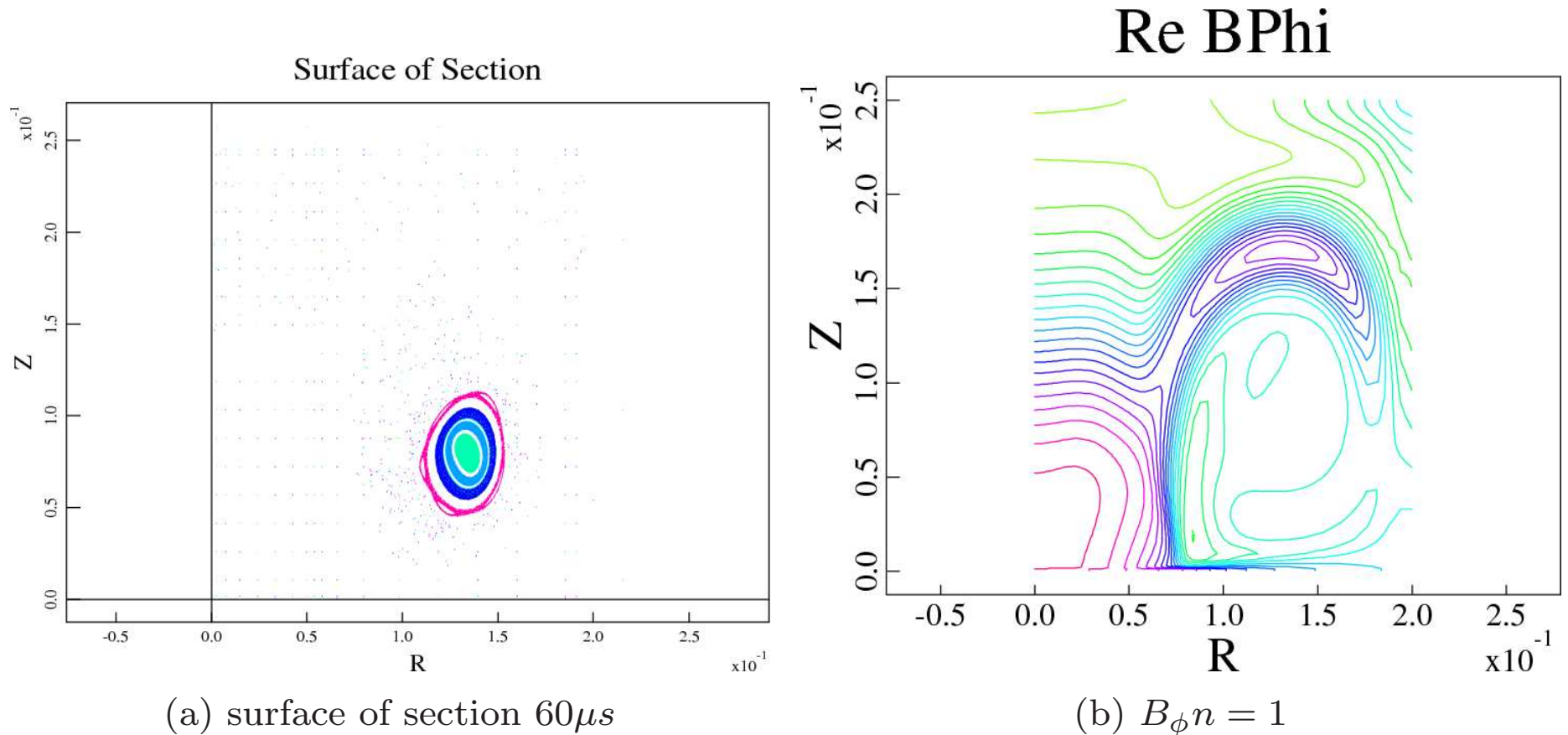
Kink and Initial Relaxed State

- current is shut off and screw pinch initialized with toroidal modes $n = [0 - 5]$
- very unstable, fast growth rate ($\sim 4.9 \times 10^7 s^{-1}$)

Magnetic Energy vs. t



- small spheromak is formed but buried by initial dipole field

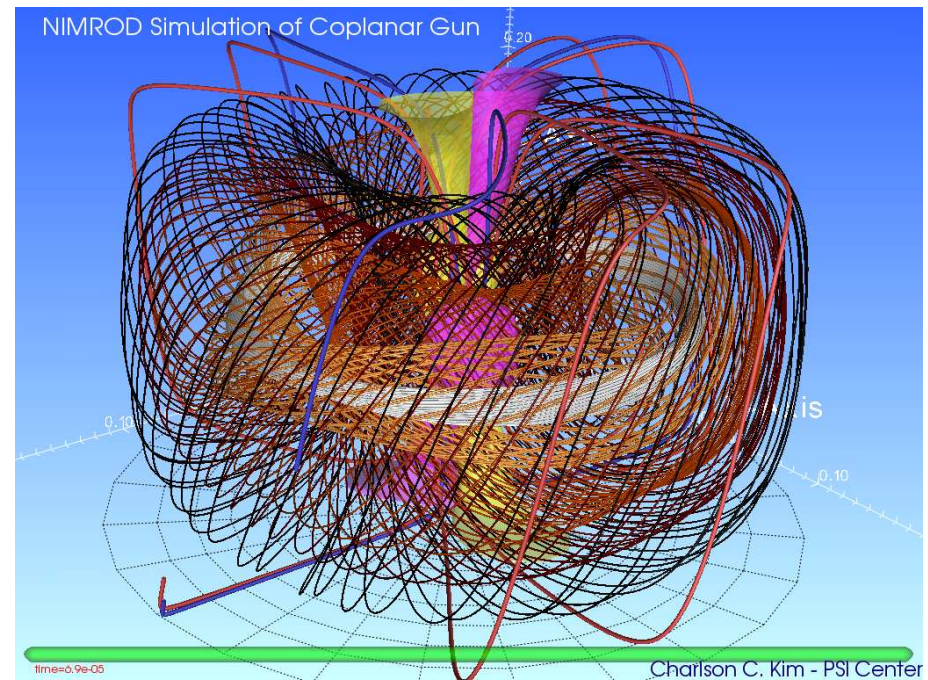
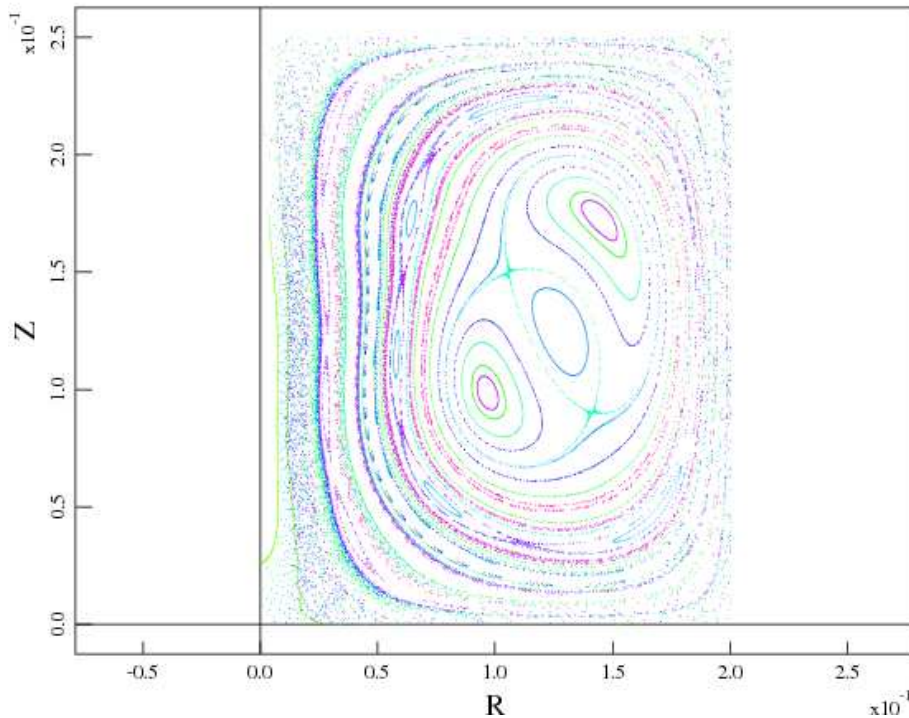


- volumetrically $n = 1$ energy is 10% of axisymmetric energy, dominantly in remnant dipole field
- quiescent in region of closed flux

Numerically 'clip' magnetic footpoints at the electrodes

- without line-tying form a robust spheromak

Surface of Section

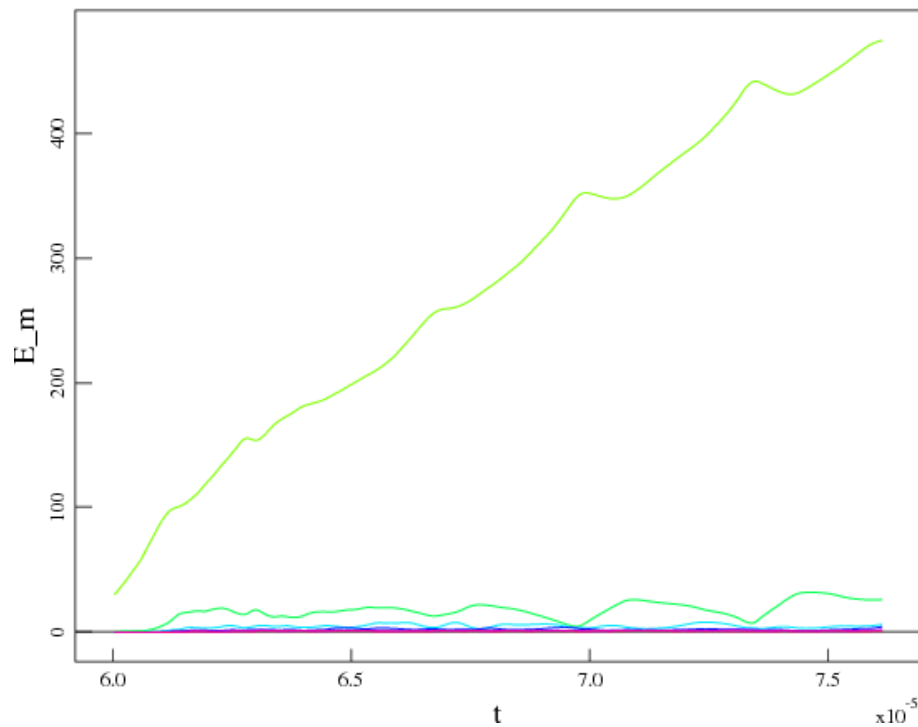


- one can infer strong impact of line tied fields

Driven Spheromak

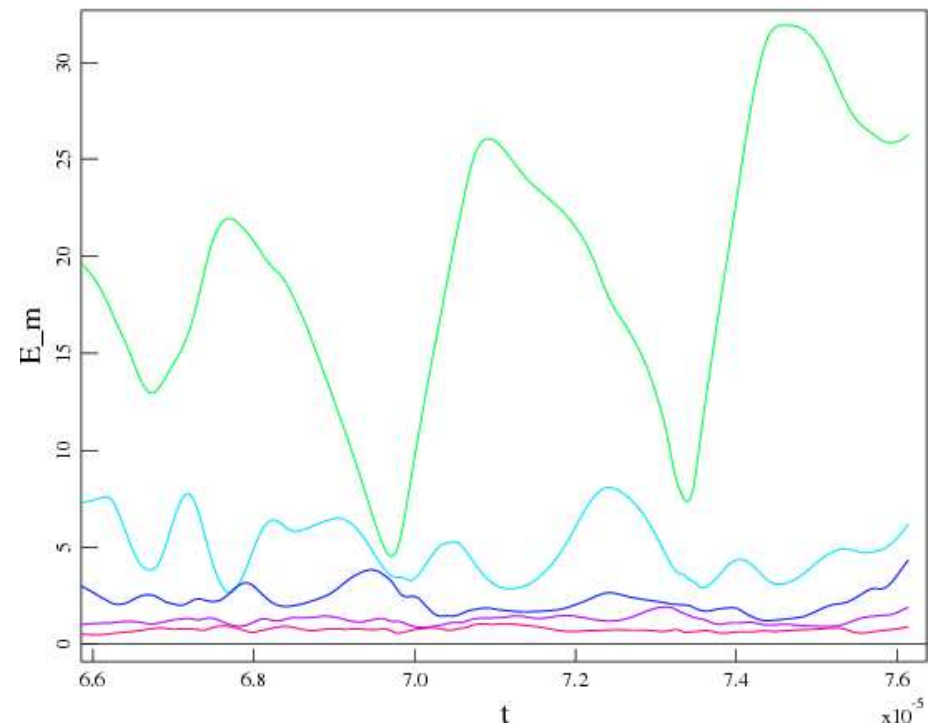
- turn the current back on - $80kA$
- observe interesting sawtooth-like behavior in $n=1$ energy

Magnetic Energy vs. t



(c) Magnetic Energy

Magnetic Energy vs. t



(d) Blowup of $n=1-5$

Second Relaxation

- two simulations with current shut off at $67.65\mu s$ and $70.9\mu s$

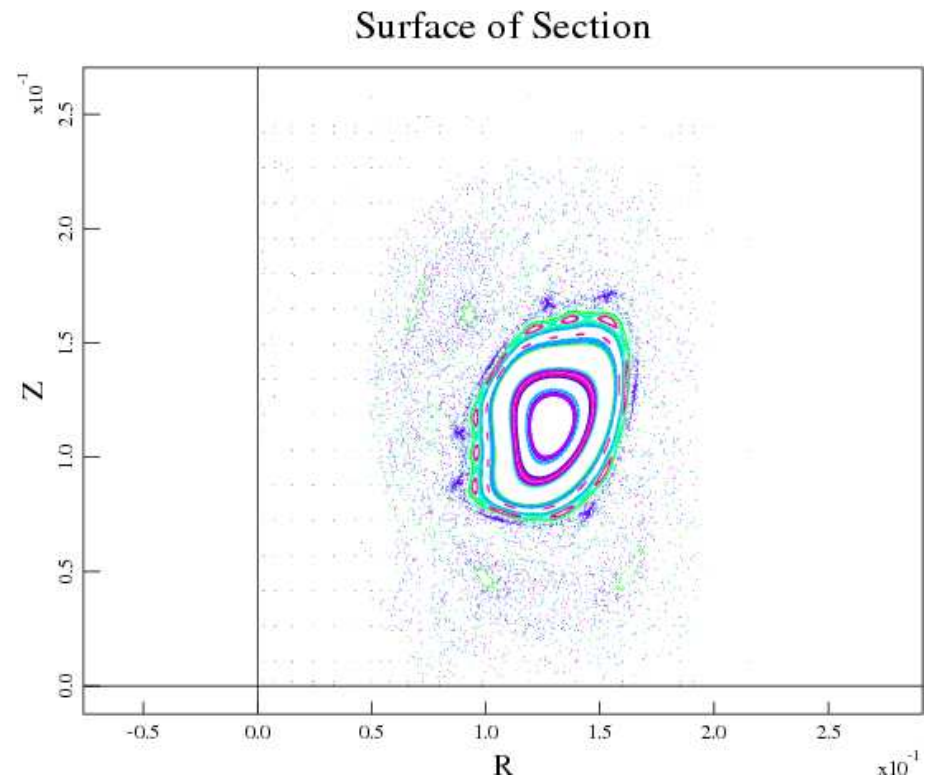
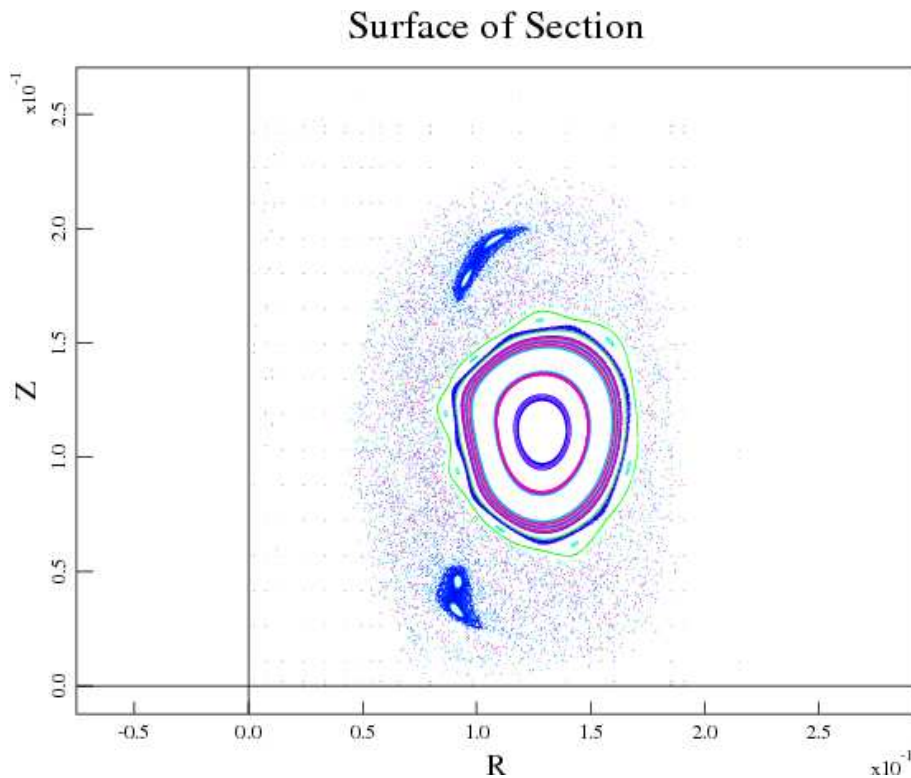


Figure 2: surface of sections $40\mu s$ after current shut off

- does it matter when the current is shut off - e.g. peak or trough

Summary

- coplanar flux injection model robust
- demonstrate formation, relaxation, drive cycle of spheromak with coplanar gun
- initial dipole field strongly impacts quality of spheromak formation
- driven spheromak exhibits sawtooth like behavior
- driven spheromaks produce larger spheromaks
- very preliminary simulations
- much more physics to turn on (compressibility, heating, 2fl, etc)