

Closure theory for high-collisionality multi-ion plasmas*

Jeong-Young Ji

Utah State University

NIMROD Team Meeting

August 2 2023, Madison WI

*PPCF **65**, 075014 (2023). Research supported by the U.S. DOE under Grant Nos. DE-SC0022048 and DE-FG02-04ER54746.

Outline

- A fluid model (5 moment, multiple species) and closures
- Moment expansion and collisional moments
- Moment equations for closures
- How to solve the moment equations: geometric method
- Electron closures for multiple ion species
- Ion closures for multiple ion species
- Deuterium-Carbon example calculations
- Convergence study by increasing the number of moments
- Two-temperature dependence of closure coefficients
- Conclusions and future work

A fluid model and closures

- Kinetic equation for a distribution function of species a , $D_a f_a = C f_a$,

$$\frac{\partial f_a}{\partial t} + \mathbf{v} \cdot \nabla f_a + \frac{q_a}{m_a} (\mathbf{E} + \mathbf{v} \times \mathbf{B}) \cdot \frac{\partial}{\partial \mathbf{v}} f_a = \sum_b C(f_a, f_b) \quad (\text{KE})$$

- Five moment (density n_a , flow velocity \mathbf{V}_a , and temperature T_a) fluid model

$$\int d^3v (\text{KE}): \quad \boxed{d_a n_a + n_a \nabla \cdot \mathbf{V}_a = 0}$$

$$\int d^3v m_a \mathbf{v} (\text{KE}): \quad \boxed{m_a n_a d_a \mathbf{V}_a - n_a q_a (\mathbf{E} + \mathbf{V}_a \times \mathbf{B}) + \nabla p_a + \nabla \cdot \boldsymbol{\pi}_a = \mathbf{R}_a}$$

$$\int d^3v \frac{1}{2} m_a w_a^2 (\text{KE}): \quad \boxed{\frac{3}{2} n_a d_a T_a + n_a T_a \nabla \cdot \mathbf{V}_a + \nabla \cdot \mathbf{h}_a + \nabla \mathbf{V}_a : \boldsymbol{\pi}_a = Q_a}$$

where $d_a = \frac{\partial}{\partial t} + \mathbf{V}_a \cdot \nabla$, $p_a = n_a T_a$, and $\mathbf{w}_a = \mathbf{v} - \mathbf{V}_a$

- Closure relations express closure variables $\{\mathbf{h}_a, \boldsymbol{\pi}_a, \mathbf{R}_a, Q_a\}$ in terms of fluid variables $\{n_a, \mathbf{V}_a, T_a\}$

Moment expansion and collisional moments

- Moment expansion in terms of irreducible tensorial Hermite polynomials \hat{p}_a^{lk}

$$f_a = f_a^M \left(1 + \sum_{lk \neq M} \hat{p}_a^{lk} \cdot \mathbf{m}_a^{lk} \right) = f_a^M [n_a, \mathbf{V}_a, T_a] + f_a^N [\mathbf{m}_a^{lk}]$$

- Closures: heat flux \mathbf{h}_a , viscosity π_a , collisional heating Q_a , and friction \mathbf{R}_a

$$\mathbf{h}_a = -\frac{\sqrt{5}}{2} n_a T_a v_{T_a} \mathbf{m}_a^{11}, \quad \pi_a = \sqrt{2} n_a T_a \mathbf{m}_a^{20}$$

$$Q_a = \sum_b \left[\frac{n_a}{\tau_{ab}} \frac{3X_{ab}^{3/2}}{\mu_{ab}} (T_b - T_a) - \sqrt{\frac{3}{2}} T_a \sum_{k=2}^{\infty} \frac{n_a}{\tau_{ab}} (a_{ab}^{01p} \mathbf{m}_a^{0k} + b_{ab}^{01p} \mathbf{m}_b^{0k}) \right]$$

$$\mathbf{R}_a = \sum_b \left[\frac{m_a n_a}{\tau_{ab}} \left(X_{ab}^{3/2} (1 + \mu_{ba}) \mathbf{V}_{ba} + \frac{v_{T_a}}{\sqrt{2}} \sum_{k=1}^{\infty} (a_{ab}^{10k} \mathbf{m}_a^{1k} + b_{ab}^{10k} \mathbf{m}_b^{1k}) \right) \right]$$

where $X_{ab}^{3/2} = (1 + \theta_{ab}/\mu_{ab})^{-1}$, $\mu_{ab} = m_b/m_a$, $\theta_{ab} = T_b/T_a$, $\mathbf{V}_{ba} = \mathbf{V}_b - \mathbf{V}_a$

- Linearized (L) collisional moments (τ_{ab} collision time)

$$\int d^3v \hat{p}_a^{lp} C (f_a^M \hat{p}_a^{lk} \cdot \mathbf{m}_a^{lk}, f_b^M) \stackrel{L}{=} \frac{n_a}{\tau_{ab}} a_{ab}^{lpk} [\mu_{ab}, \theta_{ab}] \mathbf{m}_a^{lk}$$

$$\int d^3v \hat{p}_a^{lp} C (f_a^M, f_b^M \hat{p}_b^{lk} \cdot \mathbf{m}_b^{lk}) \stackrel{L}{=} \frac{n_a}{\tau_{ab}} b_{ab}^{lpk} [\mu_{ab}, \theta_{ab}] \mathbf{m}_b^{lk}$$

Moment equations for closures

- Moment equations: take moments $\int d^3v \hat{p}_a^{lp} [D_a f_a = \sum_b C(f_a, f_b)]$

$$D_a f_a^M + D_a f_a^N = \sum_b [C(f_a^M, f_b^M) + C(f_a^N, f_b^M) + C(f_a^M, f_b^N)]$$

- For high collisionality

~~$$\left(\frac{\partial}{\partial t}, v_{Ta} \nabla, \frac{2q_a \mathbf{E}}{m_a v_{Ta}} \right) \mathbf{m}_a + \Omega_a \mathbf{b} \times \mathbf{m}_a^{lp} = \sum_b \left[\frac{1}{\tau_{ab}} \left(a_{ab}^{lpk} \mathbf{m}_a^{lk} + b_{ab}^{lpk} \mathbf{m}_b^{lk} \right) + \mathcal{G}_a^{lp} \right]$$~~

Multiply τ_{aa}

$$r_a \mathbf{b} \times \mathbf{m}_a^{lp} = \sum_b z_{ab} \left(a_{ab}^{lpk} \mathbf{m}_a^{lk} + b_{ab}^{lpk} \mathbf{m}_b^{lk} \right) + \mathbf{g}_a^{lp}$$

where $r_a = \Omega_a \tau_{aa}$ (Hall parameter), $z_{ab} = \tau_{aa} / \tau_{ab}$, and nonvanishing drives

$$\mathbf{g}_a^{1p} = \delta_{p1} \frac{\sqrt{5}}{2} \frac{n_a v_{Ta} \tau_{aa}}{T_a} \nabla T_a + \sqrt{2} n_a \sum_{b \neq a} z_{ab} b_{ab}^{1p0} \frac{\mathbf{V}_{ba}}{v_{Tb}}$$

$$\mathbf{g}_a^{20} = -\frac{1}{\sqrt{2}} n_a \tau_{aa} \mathbf{W}_a, \quad \mathbf{W}_a = \nabla \mathbf{V}_a + (\nabla \mathbf{V}_a)^T - \frac{2}{3} |\nabla \cdot \mathbf{V}_a \mathbf{I}$$

How to obtain closures: moment approach

- Moment equations for S ion species in matrix form

$$\begin{pmatrix} r_e \mathbf{b} \check{\times} m_e^l \\ r_1 \mathbf{b} \check{\times} m_1^l \\ r_2 \mathbf{b} \check{\times} m_2^l \\ r_S \mathbf{b} \check{\times} m_S^l \end{pmatrix} = \begin{pmatrix} c_e^l & 0 & 0 & 0 \\ 0 & c_1^l & c_{12}^l & c_{1S}^l \\ 0 & c_{21}^l & c_2^l & c_{2S}^l \\ 0 & c_{S1}^l & c_{S2}^l & c_S^l \end{pmatrix} \begin{pmatrix} m_e^l \\ m_1^l \\ m_2^l \\ m_S^l \end{pmatrix} + \begin{pmatrix} g_e^l \\ g_1^l \\ g_2^l \\ g_S^l \end{pmatrix}$$

$$\Rightarrow \mathbf{Rb} \check{\times} \mathbf{M}^l = \mathbf{C}^l \mathbf{M}^l + \mathbf{G}^l$$

where $c_a^{lpq} = \sum_{b=e}^S a_{ab}^{lpq} + b_{aa}^{lpq}$ and $c_{a \neq b}^{lpq} = z_{ab} b_{ab}^{lpq}$

- K -moment calculations: convergence checked by increasing K

$$m_a^0 = \begin{pmatrix} m_a^{02} \\ m_a^{03} \\ \vdots \\ m_a^{0,K+1} \end{pmatrix}, \quad m_a^1 = \begin{pmatrix} m_a^{11} \\ m_a^{12} \\ \vdots \\ m_a^{1K} \end{pmatrix}, \quad M_a^{l \geq 2} = \begin{pmatrix} m_a^{l0} \\ m_a^{l1} \\ \vdots \\ m_a^{l,K-1} \end{pmatrix}$$

- Solve the linear system for closures \mathbf{M}^l

$$\mathbf{C}^l \mathbf{M}^l - \mathbf{Rb} \check{\times} \mathbf{M}^l = -\mathbf{G}^l \Rightarrow \mathbf{M}^l = -(\mathbf{C}^l - \mathbf{Rb} \check{\times})^{-1} \mathbf{G}^l$$

How to solve the linear system $l = 1$: geometric method

- Vector decomposition $\mathbf{V} = \mathbf{V}_{\parallel} + \mathbf{V}_{\perp}$

$$\mathbf{V}_{\parallel} = b_{\parallel} \mathbf{V} = \mathbf{b} \mathbf{b} \cdot \mathbf{V}$$

$$\mathbf{V}_{\perp} = b_{\perp} \mathbf{V} = -\mathbf{b} \times (\mathbf{b} \times \mathbf{V}) = (\mathbf{I} - \mathbf{b} \mathbf{b}) \cdot \mathbf{V}$$

$$\mathbf{V}_{\times} = b_{\times} \mathbf{V} = \mathbf{b} \times \mathbf{V} = -\mathbf{V} \times \mathbf{b}$$

- Act b_{\parallel} on $C^1 M^1 - R \mathbf{b} \times M^1 = -G^1$

$$C^1 M_{\parallel}^1 = -G_{\parallel}^1 \Rightarrow M_{\parallel}^1 = -(C^1)^{-1} G_{\parallel}^1$$

- Act b_{\perp} and b_{\times} on $C M^1 - R \mathbf{b} \times M^1 = -G^1$

$$\begin{aligned} C^1 M_{\perp}^1 - R M_{\times}^1 &= -G_{\perp}^1 \\ C^1 M_{\times}^1 + R M_{\perp}^1 &= -G_{\times}^1 \end{aligned} \Rightarrow \begin{bmatrix} C^1 & -R \\ R & C^1 \end{bmatrix} \begin{bmatrix} M_{\perp}^1 \\ M_{\times}^1 \end{bmatrix} = - \begin{bmatrix} G_{\perp}^1 \\ G_{\times}^1 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} M_{\perp}^1 \\ M_{\times}^1 \end{bmatrix} = - \frac{1}{RC^1 R^{-1} C^1 + R^2} \begin{bmatrix} RC^1 R^{-1} & R \\ -R & RC^1 R^{-1} \end{bmatrix} \begin{bmatrix} G_{\perp}^1 \\ G_{\times}^1 \end{bmatrix}$$

- Solution $M^1 = M_{\parallel}^1 + M_{\perp}^1$

$$M^1 = -(C^1)^{-1} G_{\parallel}^1 - \frac{1}{RC^1 R^{-1} C^1 + R^2} (RC^1 R^{-1} G_{\perp}^1 + R G_{\times}^1)$$

How to solve the linear system $l = 2$: geometric method

- Rank-2 tensor decomposition $W = W_{\parallel\parallel} + 2W_{\parallel\perp} + W_{\perp\perp}$

$$W_{AB} = \frac{1}{2}(\mathbf{b}_A \otimes \mathbf{b}_B + \mathbf{b}_B \otimes \mathbf{b}_A)W, \text{ where } A, B = \parallel, \perp, \times$$

$$\text{e.g. } W_{\parallel\perp} = \frac{1}{2}[\mathbf{b}\mathbf{b} \cdot W \cdot (\mathbf{I} - \mathbf{b}\mathbf{b}) + (\mathbf{I} - \mathbf{b}\mathbf{b}) \cdot W \cdot \mathbf{b}\mathbf{b}]$$

$$W_{\times\times} = -\mathbf{b} \times W \times \mathbf{b}$$

- Defining $W_{(0)} = W_{\parallel\parallel} + \frac{1}{2}(W_{\times\times} + W_{\perp\perp})$, $W_{(1)} = \frac{1}{2}(W_{\perp\perp} - W_{\times\times})$,

$$W_{(2)} = 2W_{\parallel\perp}, W_{(3)} = W_{\times\perp}, W_{(4)} = 2W_{\parallel\times},$$

decompose the $l = 2$ equation $C^2M^2 - R(\mathbf{b} \times M^2 - M^2 \times \mathbf{b}) = -G^2$ into

$$C^2M_{(0)}^2 = -G_{(0)}^2$$

$$\begin{bmatrix} C^2 & -R \\ R & C^2 \end{bmatrix} \begin{bmatrix} M_{(2)}^2 \\ M_{(4)}^2 \end{bmatrix} = - \begin{bmatrix} G_{(2)}^2 \\ G_{(4)}^2 \end{bmatrix}$$

$$\begin{bmatrix} C^2 & -2R \\ 2R & C^2 \end{bmatrix} \begin{bmatrix} M_{(1)}^2 \\ M_{(3)}^2 \end{bmatrix} = - \begin{bmatrix} G_{(1)}^2 \\ G_{(3)}^2 \end{bmatrix} : \text{ same as the vector equations}$$

- Solution

$$M^2 = M_{\parallel\parallel}^2 + 2M_{\parallel\perp}^2 + M_{\perp\perp}^2 = M_{(0)}^2 + M_{(1)}^2 + M_{(2)}^2$$

Electron parallel closures for multiple ion species

- Equivalent to the theory of a single ion species with effective variables defined

$$Z = \sum_{j=\text{ions}} \frac{\tau_{ee}}{\tau_{ej}}$$

$$\frac{1}{\tau_{ei}} = \sum_{j=\text{ions}} \frac{1}{\tau_{ej}} = \frac{Z}{\tau_{ee}}$$

$$\mathbf{V}_i = \sum_{j=\text{ions}} \frac{z_{ej} \mathbf{V}_j}{Z} = \tau_{ei} \sum_{j=\text{ions}} \frac{\mathbf{V}_j}{\tau_{ej}}$$

- Electron closures for a single ion species [Braginskii 1965, Ji & Held 2013]

$$\mathbf{R}_e = \frac{m_e n_e}{\tau_{ei}} (-\hat{\alpha}_{\parallel} \mathbf{V}_{ei\parallel} - \hat{\alpha}_{\perp} \mathbf{V}_{ei\perp} + \hat{\alpha}_{\times} \mathbf{V}_{ei\times})$$

$$+ n_e (-\hat{\beta}_{\parallel} \nabla_{\parallel} T_e - \hat{\beta}_{\perp} \nabla_{\perp} T_e - \hat{\beta}_{\times} \nabla_{\times} T_e) = \sum_j \mathbf{R}_{ej} = \sum_j \frac{z_{ej}}{Z} \mathbf{R}_e$$

$$\mathbf{h}_e = n_e T_e (\hat{\beta}_{\parallel} \mathbf{V}_{ei\parallel} + \hat{\beta}_{\perp} \mathbf{V}_{ei\perp} + \hat{\beta}_{\times} \mathbf{V}_{ei\times})$$

$$+ \frac{n_e T_e \tau_{ee}}{m_e} (-\hat{\kappa}_{\parallel}^e \nabla_{\parallel} T_e - \hat{\kappa}_{\perp}^e \nabla_{\perp} T_e - \hat{\kappa}_{\times}^e \nabla_{\times} T_e)$$

$$\boldsymbol{\pi}_e = -\eta_{e(0)} \mathbf{W}_{e(0)} - \eta_{e(1)} \mathbf{W}_{e(1)} - \eta_{e(2)} \mathbf{W}_{e(2)} - \eta_{e(3)} \mathbf{W}_{e(3)} - \eta_{e(4)} \mathbf{W}_{e(4)}$$

Ion closures for multiple ion species

- Closure relations for multiple ion species ($i, j = 1, 2, \dots, S$)

$$\begin{aligned}
 \mathbf{h}_i &= \sum_j \frac{n_i T_i \tau_{jj}}{m_j} \left(-\hat{\kappa}_{\parallel,ij} \nabla_{\parallel} T_j - \hat{\kappa}_{\perp,ij} \nabla_{\perp} T_j + \hat{\kappa}_{\times,ij} \nabla_{\times} T_j \right) \\
 &\quad + n_i T_i \sum_{j,k} \left(\hat{\beta}_{\parallel,ijk}^{TV} \mathbf{V}_{\parallel,jk} + \hat{\beta}_{\perp,ij}^{TV} \mathbf{V}_{\perp,jk} - \hat{\beta}_{\times,ij}^{TV} \mathbf{V}_{\times,jk} \right) \\
 \mathbf{R}_i &= \mathbf{R}_{ie} + \sum_j n_j \left(-\hat{\beta}_{\parallel,ij}^{VT} \nabla_{\parallel} T_j - \hat{\beta}_{\perp,ij}^{VT} \nabla_{\perp} T_j + \hat{\beta}_{\times,ij}^{VT} \nabla_{\times} T_j \right) \\
 &\quad - \frac{m_i n_i}{\tau_{ii}} \sum_{j,k} \left(\hat{\alpha}_{\parallel,ijk} \mathbf{V}_{\parallel,jk} + \hat{\alpha}_{\perp,ijk} \mathbf{V}_{\perp,jk} + \hat{\alpha}_{\times,ijk} \mathbf{V}_{\times,jk} \right) \\
 \boldsymbol{\pi}_i &= p_i \sum_j \tau_{jj} \left[-\hat{\eta}_{(0)ij} \mathbf{W}_{(0)j} - \hat{\eta}_{(1)ij} \mathbf{W}_{(1)j} - \hat{\eta}_{(2)ij} \mathbf{W}_{(2)j} \right. \\
 &\quad \left. + \hat{\eta}_{(3)ij} \mathbf{W}_{(3)j} + \hat{\eta}_{(4)ij} \mathbf{W}_{(4)j} \right]
 \end{aligned}$$

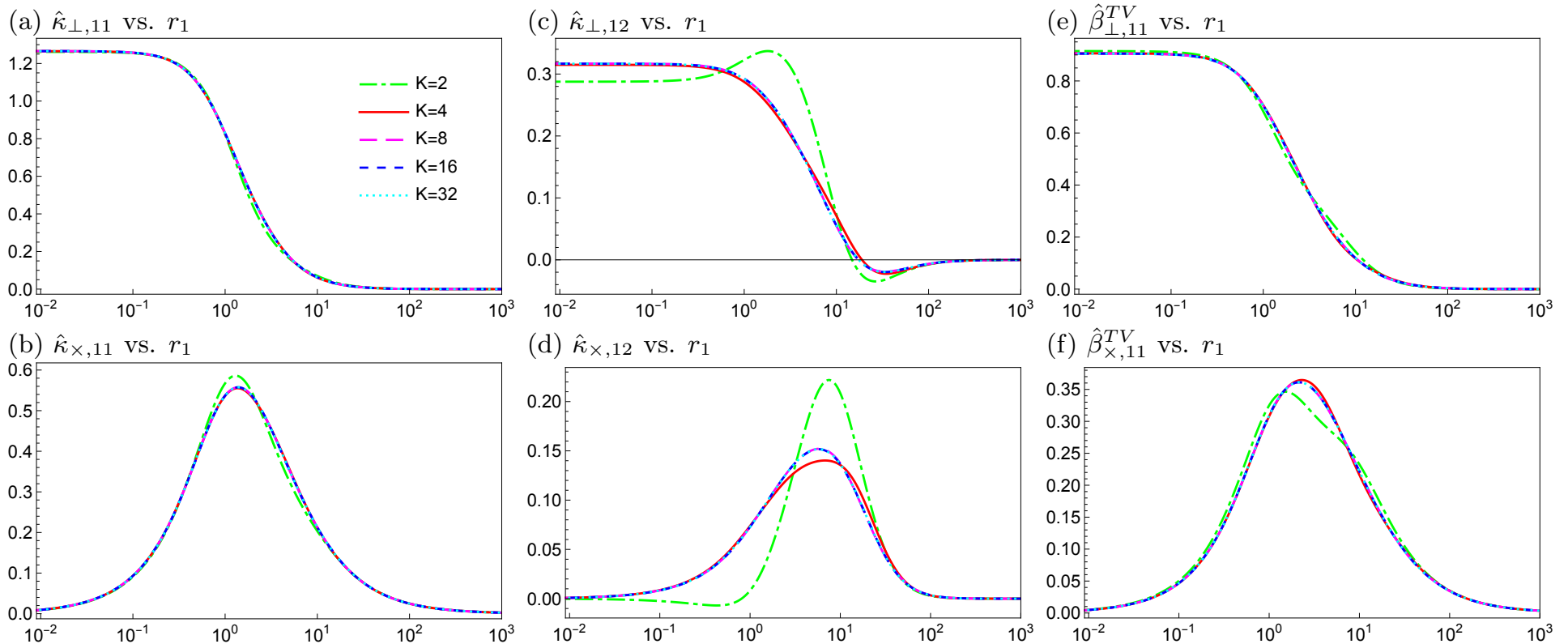
where the summation indices j and k run over ion species only

- Example study for deuterium (D) and carbon (C): $Z_D = +1$, $Z_C = +6$, $m_D = 2.014u$, $m_C = 12.00u$, $n_D = 0.64n_e$, $n_C = 0.06n_e$, $T_D = 1.5T_e$, $T_C = 1.8T_e$, and $\ln \Lambda_{ee} = 17$

Heat flux density for two ion species: convergence

Heat-flux closure coefficients of ion species 1: sum over $A = \parallel, \perp$ [$\pm = -$], \times [$+$] is implied, $\hat{\kappa}_{\parallel} = \hat{\kappa}_{\perp}(r_1 = 0)$

$$\mathbf{h}_1 = \sum_{\pm}^A \frac{n_1 T_1 \tau_{11}}{m_1} \hat{\kappa}_{A,11} \nabla_A T_1 \pm \sum_{\pm}^A \frac{n_1 T_1 \tau_{22}}{m_2} \hat{\kappa}_{A,12} \nabla_A T_2 + n_1 T_1 \hat{\beta}_{A,11}^{TV} (\mathbf{V}_1 - \mathbf{V}_2)_A$$

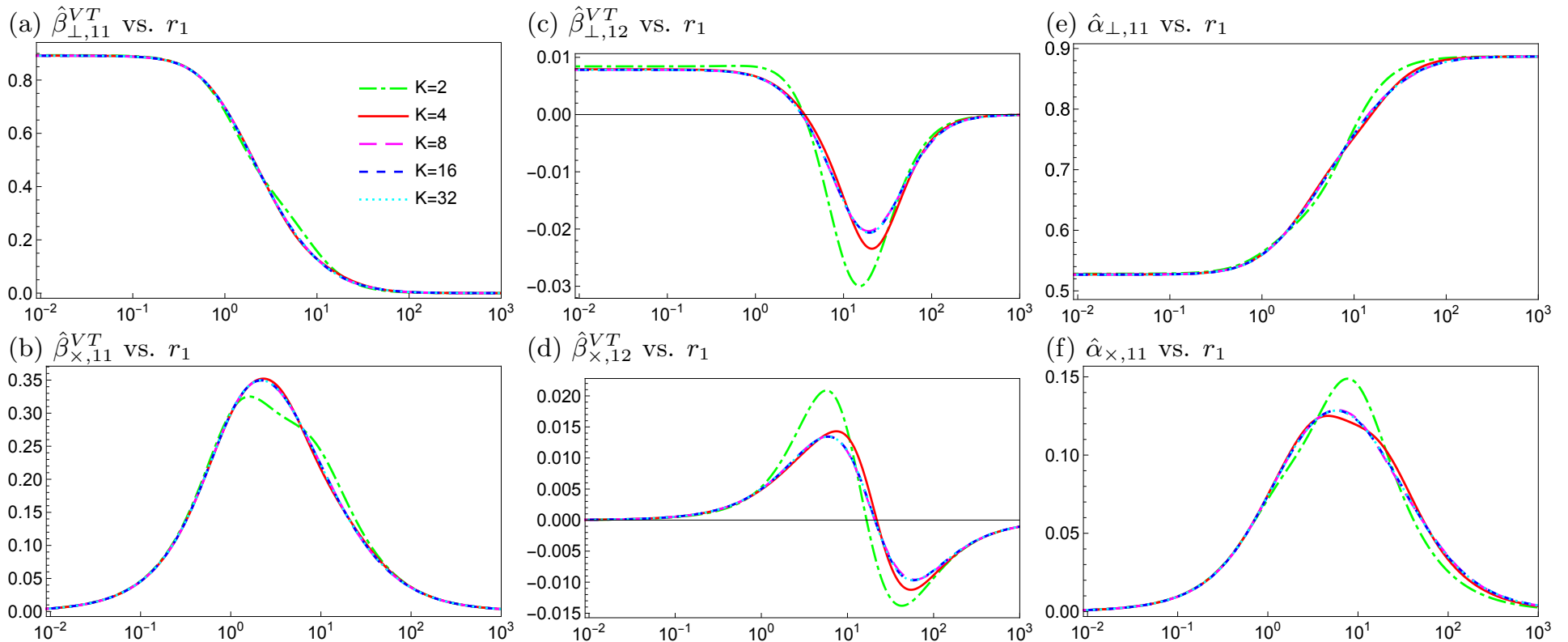


Convergent closure coefficients are obtained by increasing the number of moments from $K = 2$ to $K = 32$

Friction density for two ion species: convergence

Friction closure coefficients of ion species 1: sum over $A = \parallel, \perp$ [$- = -$], \times [$+ = +$] is implied, $\hat{\alpha}_{\parallel} = \hat{\alpha}_{\perp}(r_1 = 0)$

$$\mathbf{R}_{12} = \sum_A^{\perp, \parallel} n_1 \hat{\beta}_{A,11}^{VT} \nabla_A T_1 - \sum_A^{\perp, \parallel} n_2 \hat{\beta}_{A,12}^{VT} \nabla_A T_2 - \frac{m_1 n_1}{\tau_{11}} \hat{\alpha}_{A,11} (\mathbf{V}_1 - \mathbf{V}_2)_A$$



For the example, $K = 8$ calculations seem to yield convergent results

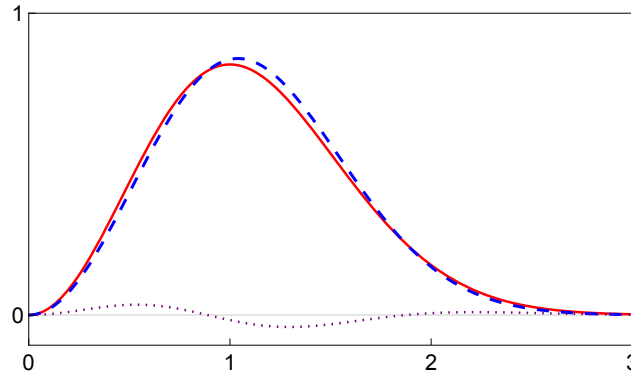
Problems of one temperature formulation $T_0 = \frac{n_a T_a + n_b T_b}{n_a + n_b}$

Moment expansion fails for $T_0 \leq T_a/2$ in the moment expansion

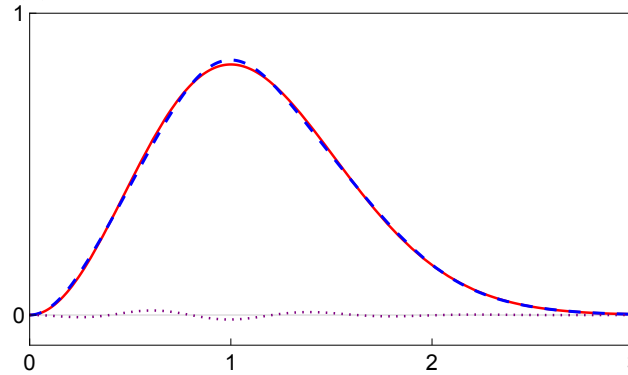
$$s_a = \frac{\mathbf{v}}{v_{T_a}} = \frac{\mathbf{v}}{\sqrt{2T_a/m_a}}, \quad s_{a0} = \frac{\mathbf{v}}{v_{T_{a0}}} = \frac{\mathbf{v}}{\sqrt{2T_0/m_a}}, \quad a_k = \left(1 - \frac{v_{T_a}^2}{v_{T_{a0}}^2}\right)^k$$

$$\frac{n_a}{\pi^{3/2} v_{T_a}^3} e^{-s_a^2} = \frac{n_a}{\pi^{3/2} v_{T_0}^3} e^{-s_{a0}^2} \left[1 + a_1 L_1^{(1/2)}(s_{a0}^2) + \dots + a_N L_N^{(1/2)}(s_{a0}^2)\right]$$

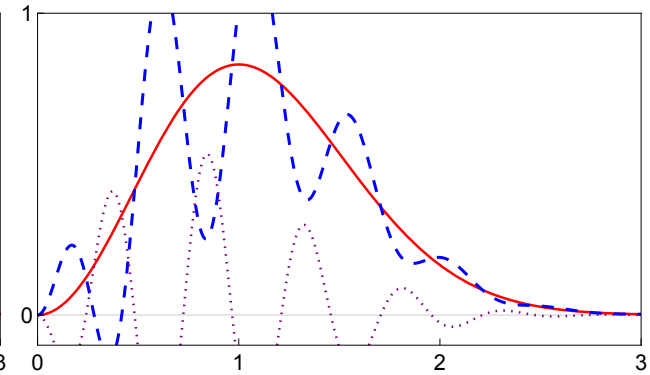
(a) $T_0 = 0.8T_a, N = 1$



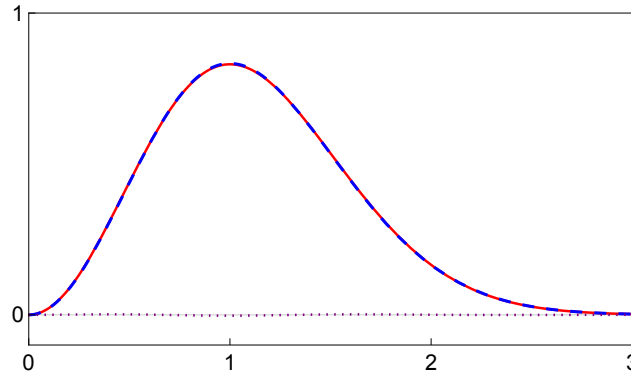
(c) $T_0 = 0.6T_a, N = 8$



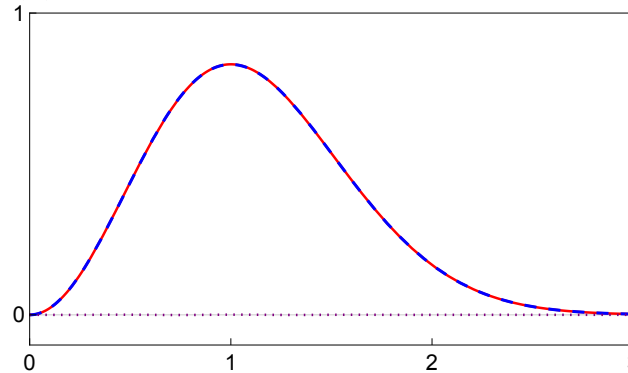
(e) $T_0 = 0.5T_a, N = 20$



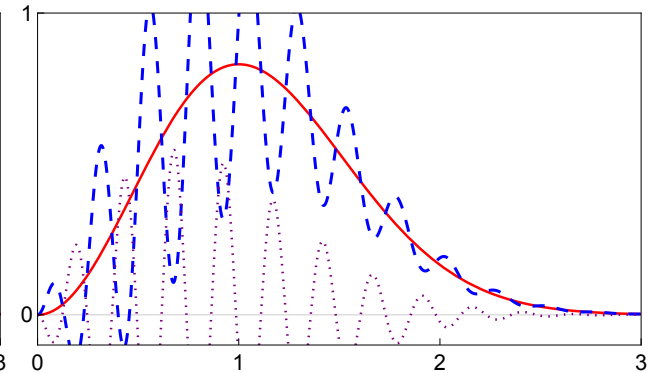
(b) $T_0 = 0.8T_a, N = 3$



(d) $T_0 = 0.6T_a, N = 16$



(f) $T_0 = 0.5T_a, N = 80$

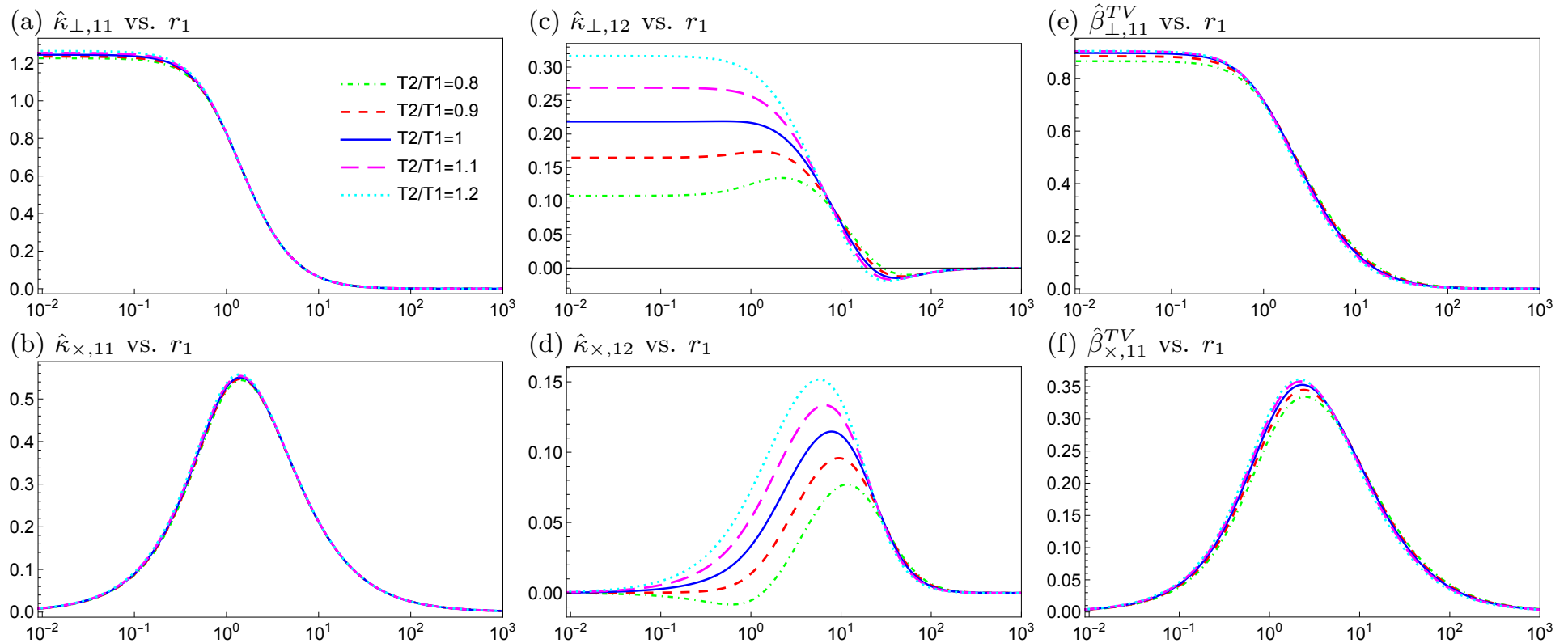


Furthermore, calculating collision coefficients with $T_a = T_b = T_0$ introduces considerable errors

Two-temperature dependence of heat flux closure coefficients

Heat-flux closure coefficients of ion species 1: sum over $A = \parallel, \perp$ [$\pm = -$], \times [$+$] is implied, $\hat{\kappa}_{\parallel} = \hat{\kappa}_{\perp}(r_1 = 0)$

$$\mathbf{h}_1 = \sum_{\pm}^A \frac{n_1 T_1 \tau_{11}}{m_1} \hat{\kappa}_{A,11} \nabla_A T_1 \pm \sum_{\pm}^A \frac{n_1 T_1 \tau_{22}}{m_2} \hat{\kappa}_{A,12} \nabla_A T_2 + n_1 T_1 \hat{\beta}_{A,11}^{TV} (\mathbf{V}_1 - \mathbf{V}_2)_A$$

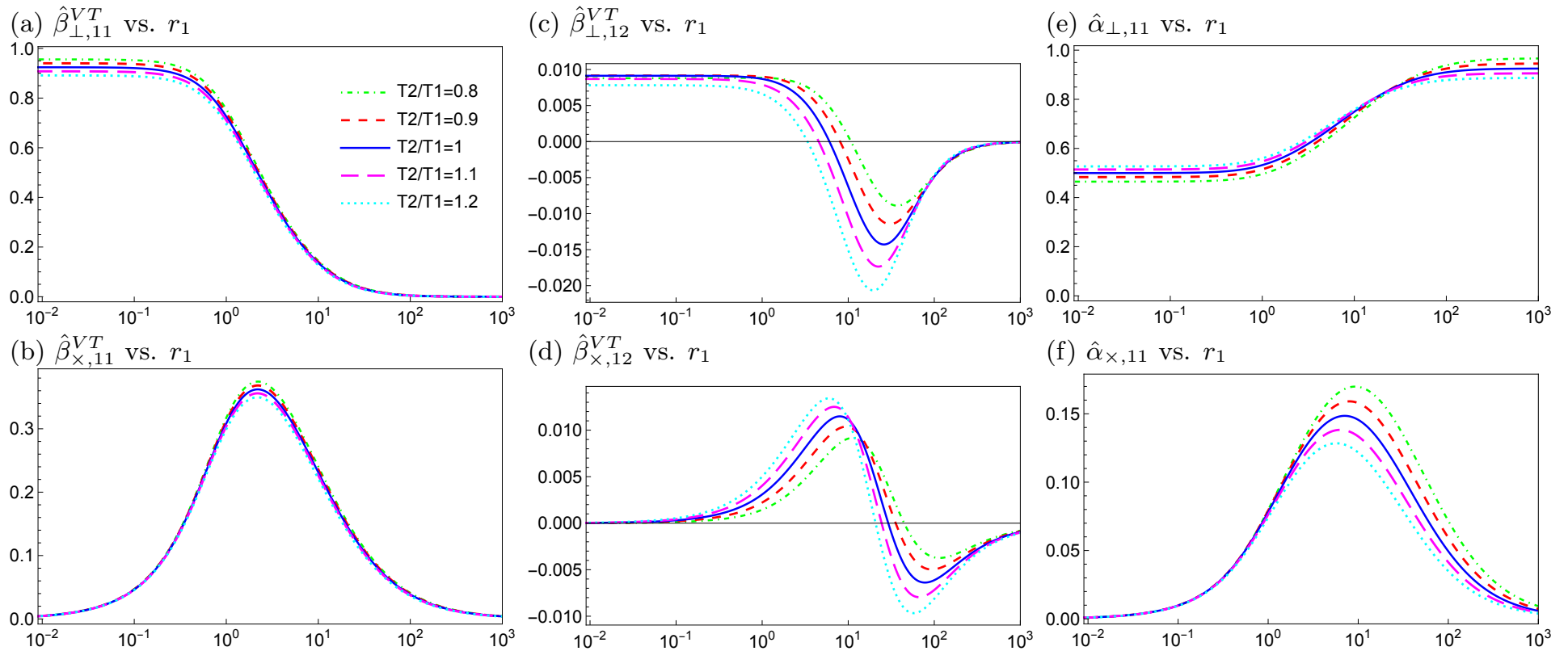


One-temperature calculations can be significantly erroneous

Two-temperature dependence of friction closure coefficients

Friction closure coefficients of ion species 1: sum over $A = \parallel, \perp$ [$- = -$], \times [$+$] is implied, $\hat{\alpha}_{\parallel} = \hat{\alpha}_{\perp}(r_1 = 0)$

$$\mathbf{R}_{12} = \sum_A^{\perp, \parallel} n_1 \hat{\beta}_{A,11}^{VT} \nabla_A T_1 \sum_A^{\perp, \parallel} n_2 \hat{\beta}_{A,12}^{VT} \nabla_A T_2 - \frac{m_1 n_1}{\tau_{11}} \hat{\alpha}_{A,11} (\mathbf{V}_1 - \mathbf{V}_2)_A$$



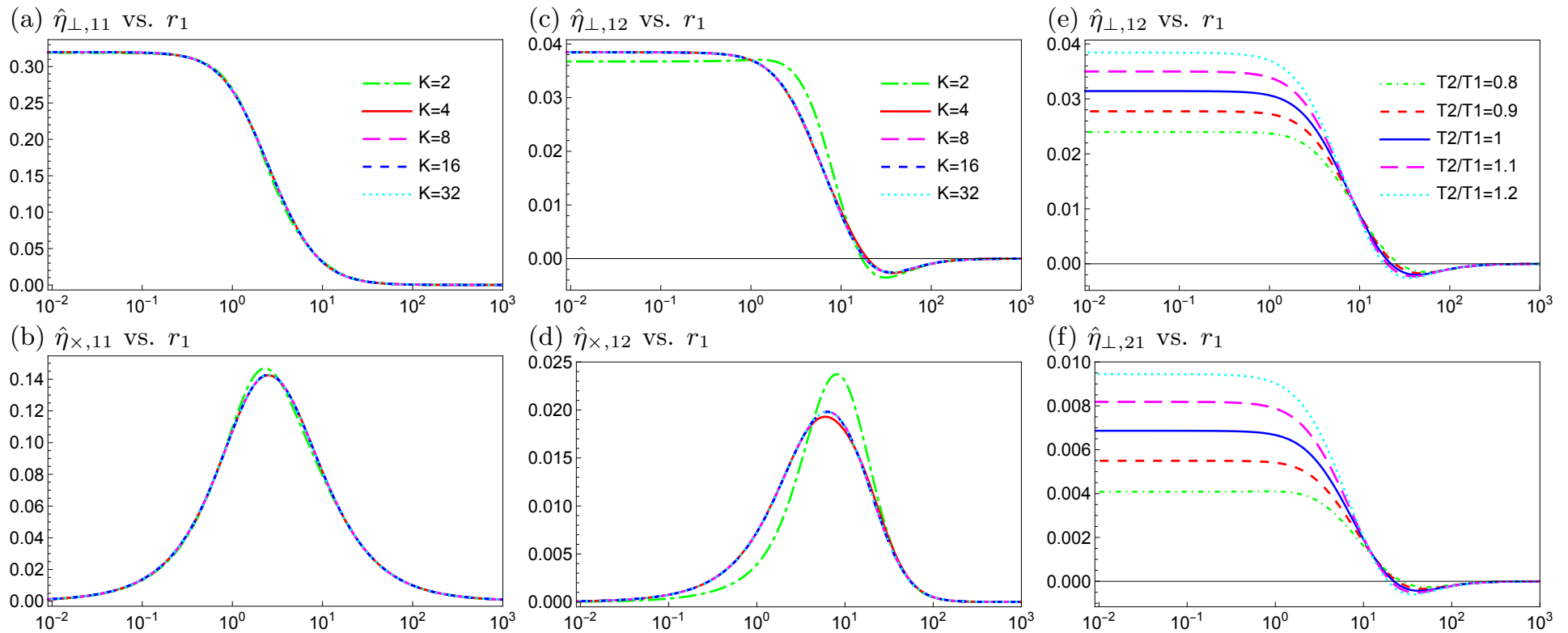
One-temperature calculations can be significantly erroneous

Viscosity closure for two ion species: convergence and two-temperature dependence

Viscosity coefficients of ion species 1: sum over $A = 0, 1, 2, [\pm = -], 3, 4[+]$ is implied

$$\hat{\eta}_{(0)} = \hat{\eta}_{\perp}(r_1 = 0), \hat{\eta}_{(1)} = \hat{\eta}_{\perp}(2r_1), \hat{\eta}_{(2)} = \hat{\eta}_{\perp}(r_1), \hat{\eta}_{(3)} = \hat{\eta}_{\times}(2r_1), \hat{\eta}_{(4)} = \hat{\eta}_{\times}(r_1)$$

$$\pi_1 = \overset{A}{\pm} p_1 \hat{\eta}_{(A),11} \tau_{11} \mathbb{W}_{(A),1} \overset{A}{\pm} p_1 \hat{\eta}_{(A),12} \tau_{22} \mathbb{W}_{(A),2}$$



Conclusions and future work

- Closure relations for multiple ion species
 - ▷ General formalism is developed for arbitrary temperatures, masses, charges, and densities
- One temperature formalism yields inaccurate results
 - ▷ Closure coefficients are sensitive to the temperature ratio
 - ▷ Moment expansion fails for $T_0 = \frac{n_a T_a + n_b T_b}{n_a + n_b} < \frac{T_a}{2}$ or $\frac{T_b}{2}$
- Machine learning can develop simple fitted coefficients for two ion species
 - ▷ Multiple ion species: find effective parameters equivalent to two ion species
- Integral parallel closures for low (arbitrary) collisionality